

3. ELECTROMAGNETIC WAVES

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2. wave equation
3. plane wave solutions
 - (a) waves are transverse
 - (b) polarization
 - (c) dispersion relation
 - (d) ratio of amplitudes of \vec{E} and \vec{B} fields (impedance)

B. PLANE WAVES IN CONDUCTORS

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 - (a) waves are transverse
 - (b) polarization
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 - (f) good and poor conductor limits

3. Electromagnetic Waves

A. Plane Waves in Dielectrics

Maxwell's equations

$$\begin{aligned} \text{div } \underline{D} &= \rho \\ \text{div } \underline{B} &= 0 \\ \text{curl } \underline{E} &= -\frac{\partial \underline{B}}{\partial t} \\ \text{curl } \underline{H} &= \underline{J} + \frac{\partial \underline{D}}{\partial t} \end{aligned}$$

(1) Maxwell's equations in dielectrics (insulators) ^{ie.}

for dielectrics: no free current, no free charge; material linear, isotropic, homogeneous

✓	↓	↓
$\underline{B} = \mu \mu_0 \underline{H}$	μ, ϵ independent of direction	μ, ϵ independent of position
$\underline{D} = \epsilon \epsilon_0 \underline{E}$		

Maxwell's equations become

$$\begin{aligned} \text{div } \underline{E} &= 0 && \textcircled{1} \\ \text{div } \underline{B} &= 0 && \textcircled{2} \\ \text{curl } \underline{E} &= -\frac{\partial \underline{B}}{\partial t} && \textcircled{3} \\ \text{curl } \underline{B} &= \mu \mu_0 \epsilon \epsilon_0 \frac{\partial \underline{E}}{\partial t} && \textcircled{4} \end{aligned}$$

(2) Wave equation

curl $\textcircled{3}$

$$\text{curl curl } \underline{E} = \text{grad div } \underline{E} - \nabla^2 \underline{E} = -\frac{\partial}{\partial t} \text{curl } \underline{B}$$

↓ zero using $\textcircled{1}$
↓ using $\textcircled{4}$

$$-\mu \mu_0 \epsilon \epsilon_0 \frac{\partial^2 \underline{E}}{\partial t^2}$$

$$\nabla^2 \underline{E} = \mu_0 \epsilon_0 \frac{\partial^2 \underline{E}}{\partial t^2}$$

(taking curl ④ gives an identical equation for \underline{B})

wave equation: solutions have a speed of propagation

$$v = \frac{1}{(\mu_0 \epsilon_0)^{1/2}}$$

in free space $v \equiv c = \frac{1}{(\mu_0 \epsilon_0)^{1/2}}$

↑
velocity of light, which is part of the e.m. spectrum

refractive index n defined by

$$n = \frac{c}{v} = (\mu \epsilon)^{1/2}$$

(NB in general n depends on ω)

(3) plane wave solutions

choose \hat{z} to define direction of propagation

plane wave means $\frac{\partial}{\partial x} = 0$, $\frac{\partial}{\partial y} = 0$

(a) plane waves are transverse

$$\textcircled{1} \Rightarrow \frac{\partial E_z}{\partial z} = 0$$

$$\textcircled{2} \Rightarrow \frac{\partial B_z}{\partial z} = 0$$

$$\textcircled{3} \Rightarrow \frac{\partial B_z}{\partial t} = 0$$

$$\textcircled{4} \Rightarrow \frac{\partial E_z}{\partial t} = 0$$

\therefore all derivatives of E_z, B_z zero $\therefore E_z, B_z$ constant and not part of any wave motion \therefore wave transverse

(b) polarization

x and y components of (3)

$$-\frac{\partial E_y}{\partial z} = -\frac{\partial B_x}{\partial t} \quad (5a) \quad \frac{\partial E_x}{\partial z} = -\frac{\partial B_y}{\partial t} \quad (5b)$$

x and y components of (4)

$$-\frac{\partial B_y}{\partial z} = \mu_0 \epsilon_0 \frac{\partial E_x}{\partial t} \quad (6a) \quad \frac{\partial B_x}{\partial z} = \mu_0 \epsilon_0 \frac{\partial E_y}{\partial t} \quad (6b)$$

solving (5a), (6b) will give a solⁿ for B_x, E_y

" (5b), (6a) " " " " " " B_y, E_x

two independent solutions with $\underline{B}, \underline{E}$ and the direction of propagation (\hat{z}) mutually orthogonal

The direction of the \underline{E} -field is taken to define the polarization of the wave. Here we have two plane polarised solutions.

(c) dispersion relation

For plane waves of a single frequency ω , with \underline{E} polarised along \hat{x}

$$\underline{E}(z, t) = E_0 e^{j(\omega t + kz)}$$

$$\underline{B}(z, t) = B_0 e^{j(\omega t - kz)}$$

wave travelling towards +ve \hat{z}

wave travelling towards -ve \hat{z}

$$\textcircled{5b} \Rightarrow \mp k E_0 = -\omega B_0 \quad \textcircled{7}$$

$$\textcircled{6a} \Rightarrow \pm k B_0 = \mu_0 \epsilon_0 \omega E_0 \quad \textcircled{8}$$

these equations are consistent if

$$\frac{\omega^2}{k^2} = \frac{1}{\epsilon_0 \mu_0} \equiv v^2$$

speed $\therefore v = \frac{1}{(\mu_0 \epsilon_0)^{1/2}}$

(as we already knew; from properties of the wave equation)

(d) ratio of the amplitudes of \underline{E} and \underline{B} fields

from $\textcircled{7}$ or $\textcircled{8}$

$$\frac{E_0}{B_0} = \pm \frac{\omega}{k} = \pm \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

$$\text{Impedance } Z \equiv \frac{E_0}{H_0} = \frac{\mu_0 E_0}{B_0} = \pm \sqrt{\frac{\mu_0}{\epsilon_0}}$$

wave moving towards \hat{z} Z +ve
 $-\hat{z}$ Z -ve

$$\text{Impedance of free space } Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 \Omega$$

B. Plane Waves in Conductors

(1) Maxwell's equations

no free charge

linear, isotropic, homogeneous material $\therefore \underline{D} = \epsilon\epsilon_0 \underline{E}$; $\underline{B} = \mu\mu_0 \underline{H}$

$$\underline{J} = \sigma \underline{E} \quad \text{Ohm's law}$$

↑ conductivity (material property)

Maxwell's equations become

$$\text{div } \underline{E} = 0 \quad (1)$$

$$\text{div } \underline{B} = 0 \quad (2)$$

$$\text{curl } \underline{E} = - \frac{\partial \underline{B}}{\partial t} \quad (3)$$

$$\text{curl } \underline{B} = \mu\mu_0 \sigma \underline{E} + \mu\mu_0 \epsilon\epsilon_0 \frac{\partial \underline{E}}{\partial t} \quad (4)$$

(2) Good and poor conductors

(a) decay of an inhomogeneous charge distribution vs period of e.m. wave

If there is a charge distribution $\rho_f(0)$ in a conductor at $t=0$, how quickly does it decay to zero?

continuity equation

$$\text{div } \underline{J} = - \frac{\partial \rho}{\partial t}$$

Ohm's law

$$\sigma \text{ div } \underline{E}$$

Gauss' law

N.B.
 σ conductivity
 ρ volume charge density

$$\frac{\sigma \rho}{\epsilon \epsilon_0} = - \frac{\partial \rho}{\partial t}$$

$$\therefore \rho(t) = \rho(0) e^{-\frac{\sigma t}{\epsilon \epsilon_0}}$$

characteristic decay time $\tau = \frac{\epsilon \epsilon_0}{\sigma}$

σ large $\Rightarrow \tau$ small ✓

ϵ large \Rightarrow field gradients smaller $\Rightarrow \tau$ longer ✓

if an e.m. wave of frequency ω is passing through the conductor the other time scale is ω^{-1}

charge distribution $\omega^{-1} \gg \tau$
 can keep up with fields

$$\frac{\sigma}{\omega \epsilon \epsilon_0} \gg 1$$

good conductor

charge distribution $\omega^{-1} \ll \tau$
 can't keep up with fields

$$\frac{\sigma}{\omega \epsilon \epsilon_0} \ll 1$$

poor conductor

(b) conduction vs displacement currents
comparing to Maxwell (4)

$$\therefore \text{curl } \underline{B} = \mu_0 \sigma \underline{E} + \mu_0 \epsilon \epsilon_0 \frac{\partial \underline{E}}{\partial t}$$

↑
conduction
current

↑
displacement
current

for a wave $\sim e^{j\omega t}$

$$\frac{\text{conduction current}}{\text{displacement current}} \sim \frac{\sigma}{\epsilon \epsilon_0 \omega}$$

∴ good conductor conduction current \gg displacement current
 poor conductor " \ll "

(c) numbers

	crossover frequency between good and poor conductor $\omega^* \sim \frac{\sigma}{\epsilon \epsilon_0}$	$\omega^* \text{ (s)}^{-1}$	ϵ	$\omega^* \text{ (s)}^{-1} \epsilon \epsilon_0$
typical metal	5×10^7		~ 1	10^{19}
graphite	7×10^4		~ 1	10^{16}
salt water	20		80	10^{10}
silicon	4×10^{-4}		12	10^7
pure water	4×10^{-6}		80	10^4
typical insulator (e.g. wood, glass)	10^{-10}		5	10

$$\therefore \underline{E}(z, t) = E_0 e^{-xz} e^{j(\omega t - kz)} \quad \hat{z} \quad (6)$$

$$\underline{B}(z, t) = B_0 e^{-xz} e^{j(\omega t - kz)} \quad \hat{y}$$

definitions: $v = \frac{\omega}{k}$

refractive index $n = \frac{ck}{\omega}$

complex refractive index $\tilde{n} = \frac{ck}{\omega}$

skin depth $\delta = \kappa^{-1}$ (length over which amplitude decays by a factor e^{-1})

subst (6) into the wave eqⁿ (5)

$$(x + jk)^2 = j\mu_0 \sigma \omega - \mu_0 \epsilon \epsilon_0 \omega^2$$

$$\therefore \kappa^2 - k^2 = -\mu_0 \epsilon \epsilon_0 \omega^2 \quad (7) \quad 2kx = j\mu_0 \sigma \omega \quad (8)$$

eliminating k
subst. (8) into (7) to get a quadratic for κ^2 ; solve and take $\sqrt{\quad}$ to give

$$\kappa = \sqrt{\frac{\mu_0 \epsilon \epsilon_0 \omega^2}{2} \left\{ \sqrt{1 + \left(\frac{\sigma}{\epsilon \epsilon_0 \omega}\right)^2} - 1 \right\}^{\frac{1}{2}}} \quad (9)$$

$$k = \sqrt{\frac{\mu_0 \epsilon \epsilon_0 \omega^2}{2} \left\{ \sqrt{1 + \left(\frac{\sigma}{\epsilon \epsilon_0 \omega}\right)^2} + 1 \right\}^{\frac{1}{2}}}$$

N.B. always take $\sqrt{\quad}$ so that κ +ve

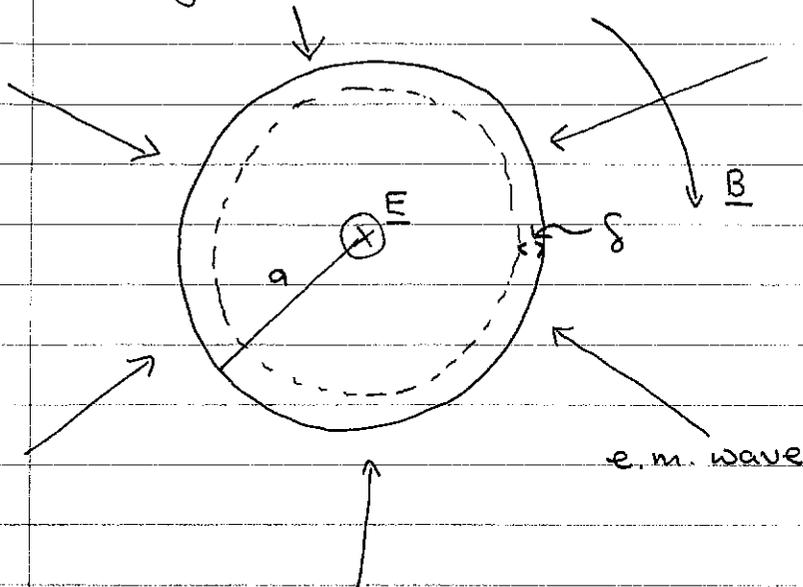
N.B. take $+$ $\sqrt{\quad}$ for wave travelling to $+\hat{z}$

(d) skin depth $\delta = \kappa^{-1}$

For a typical metal in the visible $\delta \sim \text{few nm}$

microwave $\sim \mu\text{m}$

radius $\sim \text{mm}$



current carried very near surface of wire

N.B. 1. $\delta \sim \omega^{-1/2}$ for a good conductor \therefore d.c. limit sensible

$$2. \text{ resistance } R = \frac{l}{A\sigma} \quad \therefore \frac{R_{ac}}{R_{dc}} \sim \frac{A_{dc}}{A_{ac}} \sim \frac{\pi a^2}{2\pi a \delta} = \frac{a}{2\delta}$$

\therefore a.c. resistance \gg d.c. resistance

3. for insulators; δ independent of ω and \gg dimensions of any sensible wire

(e) ratio of amplitudes of \underline{E} and \underline{B} - fields

Maxwell ③, taking y-component of curl,

$$\frac{\partial E_{zc}}{\partial z} = - \frac{\partial B_y}{\partial t}$$

substituting in the plane wave solⁿ ⑥

$$- (k + jk) E_0 = - j\omega B_0$$

$$\therefore B_0 = \frac{(k + jk) E_0}{j\omega}$$

$$\uparrow Z = \frac{\mu\mu_0 E_0}{B_0} = \frac{\mu\mu_0 \omega}{k - jk} \equiv Z_0 e^{+j\phi}$$

Complex
impedance

$$\text{where } Z_0 = \mu\mu_0 \left| \frac{E_0}{B_0} \right| = \frac{\mu\mu_0 \omega}{(c^2 + k^2)^{1/2}}$$

$$\therefore \tan \phi = \frac{x}{k} = \left\{ \frac{\sqrt{1 + \left(\frac{\sigma}{\epsilon\epsilon_0 \omega}\right)^2} - 1}{\sqrt{1 + \left(\frac{\sigma}{\epsilon\epsilon_0 \omega}\right)^2} + 1} \right\}^{1/2}$$

(f) Limits(i) 'good' conductor $\frac{\sigma}{\epsilon \epsilon_0 \omega} \gg 1$

$$\therefore k = \kappa = \sqrt{\frac{\mu \mu_0 \epsilon \epsilon_0 \omega^2 \sigma}{2 \epsilon \epsilon_0 \omega}} = \sqrt{\frac{\mu \mu_0 \omega \sigma}{2}}$$

IMPORTANT N.B.

To work out the dispersion relation or skin depth of a good conductor can derive the general formula⁽⁹⁾ for κ , k and then approximate

but unless you need the general formula for some other reason it is much easier to approximate earlier e.g. in (5)

$$(5) \Rightarrow \nabla^2 \underline{E} = \mu \mu_0 \sigma \frac{\partial \underline{E}}{\partial t} + \cancel{\mu \mu_0 \epsilon \epsilon_0 \frac{\partial^2 \underline{E}}{\partial t^2}}$$

↑
negligible for a good conductor

substituting in the plane wave solution (6)

$$\underline{E}(z, t) = E_0 e^{-\kappa z} e^{j(\omega t - kz)} \hat{x}$$

gives the good conductor dispersion relation

$$(k + j\kappa)^2 = j\mu \mu_0 \sigma \omega$$

equating real and imaginary parts

$$\therefore k^2 - \kappa^2 = 0 \quad (\text{cf } (7))$$

$$2k\kappa = \mu \mu_0 \sigma \omega \quad (\text{cf } (8))$$

$$\therefore k = \kappa = \sqrt{\frac{\mu \mu_0 \sigma \omega}{2}} \quad (\text{as before})$$

(ii) 'poor' conductor

$$\frac{\sigma}{\epsilon \epsilon_0 \omega} \ll 1$$

$$K = \sqrt{\frac{\mu \mu_0 \epsilon \epsilon_0 \omega^2}{2} \left(1 + \frac{\sigma^2}{2(\epsilon \epsilon_0 \omega)^2} - 1 \right)^{1/2}}$$

$$= \sqrt{\frac{\mu \mu_0 \epsilon \epsilon_0}{2 \cdot 2}} \cdot \omega \cdot \frac{\sigma}{\epsilon \epsilon_0 \omega} = \frac{\sigma}{2} \sqrt{\frac{\mu \mu_0}{\epsilon \epsilon_0}}$$

skin depth
of a poor
conductor is
independent of
 ω

$$R = \sqrt{\frac{\mu \mu_0 \epsilon \epsilon_0}{2}} \cdot \omega \sqrt{2} \left(1 + \frac{\sigma^2}{4(\epsilon \epsilon_0 \omega)^2} \right)^{1/2}$$

$$= \omega \sqrt{\mu \mu_0 \epsilon \epsilon_0} \left(1 + \frac{\sigma^2}{8(\epsilon \epsilon_0 \omega)^2} \right)$$

↑
can ignore of

(iii) dielectric $\sigma = 0$ $K = 0$ ✓

$$R = \omega \cdot \frac{1}{\nu} \quad \checkmark$$