

5. Braginskii MHD.

In this last part of the course, I will expand the tentative transport calculations which started with resistivity etc. and show you how to calculate the friction force (so resistivity), the heat fluxes, and the momentum fluxes in a plasma embedded in a magnetic field - effectively, we will be arranging a marriage between K-MHD and collisions.

All this is based on seminal paper by Braginskii (1965), which proved that one could become eternally famous by being the first to do a standard but very difficult calculation properly. This is called "classical transport". In fusion science, ~~this~~ this was followed by decades of "neoclassical transport" (one featuring trapped-particle physics in curved fields) - you will find an intro to that in F. Parra's notes (and while Braginskii is their patron saint, Felix is the reigning emperor of the neoclassical calculators - a joint emperor with Per Helander perhaps, whose book is the bible of the field). Sadly, I will not have time to cover neoclassical transport.

5.1 Collisional contributions to electron distribution function

Let us recall how electrons ~~particles~~ were described in ~~our~~ our derivation of KMH.D.

$$\text{From } \frac{\partial f_e}{\partial t} + \vec{v} \cdot \nabla f_e - \frac{e}{m_e} (\vec{E} + \frac{\vec{v} \times \vec{B}}{c}) \cdot \frac{\partial f_e}{\partial \vec{v}} = \left(\frac{\partial f_e}{\partial t} \right)_c \quad (239)$$

we go to $\vec{v} = \vec{w} + \vec{u}_e$ and so

$$\frac{df_e}{dt_e} + \vec{w} \cdot \nabla f_e + \left(-\frac{e}{m_e} \frac{\vec{w} \times \vec{B}}{c} - \vec{w} \cdot \nabla \vec{u}_e + \vec{a}_e \right) \cdot \frac{\partial f_e}{\partial \vec{w}} = \left(\frac{\partial f_e}{\partial t} \right)_c \quad (240)$$

$\frac{\partial}{\partial t} + \vec{u}_e \cdot \nabla$
 $\left(-\frac{e}{m_e} \left(\frac{\partial f_e}{\partial \vec{w}} \right)_{w_i, w_j} \right)$

 $\left(-\frac{e}{m_e} (\vec{E} + \frac{\vec{u}_e \times \vec{B}}{c}) - \frac{d\vec{u}_e}{dt_e} \right)$

$s_e < 0!!!$ forces in a frame moving with \vec{u}_e

This distribution function now is required to satisfy $\int d\vec{w} \vec{w} f_e = 0$ (241), whereas \vec{u}_e is found from the momentum equation

$$-m_e n_e \vec{a}_e = -\nabla \cdot \hat{P}_e + \vec{R}_{ei} \quad (242)$$

↑ friction force

For electrons, because m_e is small, we usually trick of the momentum equation as the equation for the Electric field - generalized Ohm's law:

$$\vec{E} = -\frac{\vec{u}_e \times \vec{B}}{c} - \frac{m_e}{e} \frac{d\vec{u}_e}{dt} - \frac{\nabla \cdot \hat{P}_e}{ene} + \frac{\vec{R}_{ei}}{ene} \quad (243)$$

$-\frac{\vec{u}_e \times \vec{B}}{c}$ $+$ $\frac{\vec{j} \times \vec{B}}{cem_e}$ ↑ electron inertia ↑ "Hall term" ↑ "nonohmic term" ↑ friction force ("Ohmic")

↑ \vec{E} field in fluid frame

$$\vec{R}_{ei} = \int d\vec{w} m_e \vec{w} \left(\frac{\partial f_e}{\partial t} \right)_c$$

When deriving ideal MHD, or KMHD, one argues all these terms (except \vec{u}_i) to be small in the Larmor-radius expansion - it is those terms that people interested in non-MHD reconnection focus on (some of them - Hall, lowest-order-in- $k\rho_e$ parts of $\nabla \cdot \hat{P}_e$ - do not in fact break flux conservation, but can modify the structure and dynamics of reconnecting sheets; others can step in do resistivity's job - electron inertia, FLR terms in \hat{P}_e . The simplest, I think, introduction this kind of physics is the appendix of the paper by Zocco & AAS-2011).

The grounds for neglecting \vec{P}_e in (243) is that

$$\frac{v_{ei}}{\Omega_e} \ll 1, \text{ but we already know, from reconnection}$$

experience, that ideal MHD will always find a way to access resistivity. Let us now allow it to do this formally by ordering

$$\boxed{\frac{v_{ei}}{\Omega_e} \sim 1} \quad \text{~~is not~~}$$

We will, however, continue assuming $\frac{\omega}{\Omega_e} \ll 1$, i.e.,

$$\boxed{\omega \sim k u_e \sim k v_{the} \ll \Omega_e \sim v_{ei}} \quad (244)$$

↑ in fact $\ll 1$ because we will assume

$$u_e \sim u_i \sim v_{thi} \ll v_{the} \text{ in the } \sqrt{m_e/m_i} \text{ expansion}$$

~~The result of this is that in our derivations, the argument is now $\omega \ll \Omega_e$.~~

With this ordering, the collision term is as large as the Ω_e term:

$$\Omega_e \left(\frac{\partial f_e}{\partial t} \right)_{w_L, w_{||}} + \left(\frac{\partial f_e}{\partial t} \right)_c = \frac{df_e}{dt_e} + \vec{w} \cdot \nabla f_e + (\vec{a}_e - \vec{w} \cdot \nabla \vec{u}_e) \cdot \frac{\partial f_e}{\partial \vec{w}}$$

Annotations and simplifications:

- $\frac{\omega}{\Omega_e} \sim \frac{k v_{the}}{\Omega_e} \sim k \rho_e \sqrt{\frac{m_e}{m_i}}$ (assuming $u_e \sim v_{the}$)
- $\frac{k v_{the}}{\Omega_e} \sim k \rho_e$
- $\frac{\nabla \cdot \vec{P}_e - \vec{R}_{ei}}{m_e n_e} \sim \frac{k \rho_e}{m_e n_e v_{the} \Omega_e} \sim \frac{k \rho_e}{m_e n_e v_{the} \Omega_e} \sim k \rho_e$
- $\frac{\vec{v}_{ei} u_e}{\Omega_e v_{the}} \sim \frac{v_{ei}}{\Omega_e} \sqrt{\frac{m_e}{m_i}}$
- $\frac{k v_{the}}{\Omega_e} \sim k \rho_e \sqrt{\frac{m_e}{m_i}}$

From (242): $\frac{\nabla \cdot \vec{P}_e - \vec{R}_{ei}}{m_e n_e}$

We have several small parameters,
So let us keep careful track:

$k \rho_e, \sqrt{\frac{m_e}{m_i}}, \frac{v_{ei}}{\Omega_e} \sim L$ for now but
we will have an subsidiary
expansion in it before long!

Formally, let us order $k \rho_e \sim \sqrt{\frac{m_e}{m_i}}$ and banish forever (246)

the 2nd-order terms — e. inertia $\frac{df_e}{dt_e}$ and the

"Coriolis force" $\vec{w} \cdot \nabla \vec{u}_e$

$$\Omega_e \left(\frac{\partial f_e}{\partial t} \right)_{w_L, w_{||}} + \left(\frac{\partial f_e}{\partial t} \right)_c = \vec{w} \cdot \nabla f_e + \vec{a}_e \cdot \frac{\partial f_e}{\partial \vec{w}} \quad (247)$$

0th order 1st order

5.1.1 Φ -th order

= 0 to lowest order.

The Φ -th order solution is now not simply a gyrotopic function but a Maxwellian:

$$\left(\frac{\partial f_e}{\partial t} \right)_c = v_D L[f_e] + \left(\frac{\partial f_e}{\partial t} \right)_e \quad (248)$$

\uparrow enforces isotropy in \vec{u}_e frame \uparrow enforces Maxwellianity in \vec{u}_e frame.

Since we are working to lowest order in $\sqrt{\frac{m_e}{m_i}}$, the difference between the \vec{u}_i and \vec{u}_e frames does not matter at this order (but will matter at the next one!)

Formally, you might ask for a proof that the Maxwellian is the only solution. That's easy:

$\int d\vec{w}$ (247) $\cdot (1 + \ln f_0)$ gives (to lowest order)

$$\int d\vec{w} \left(\frac{\partial}{\partial \vec{v}} f_0 \ln f_0 \right)_{w_{\perp}, w_{\parallel}} + \int d\vec{w} \ln f_0 \left(\frac{\partial f_0}{\partial t} \right)_e = 0 \quad (249)$$

$\underbrace{\int d\vec{w}}_{\substack{\parallel \\ 0}} \int dw_{\perp} dw_{\parallel} d\vec{v}$

\uparrow
 Vanishes iff f_0 is a local Maxwellian (as in the proof of the H theorem)

So, we have

$$f_e = f_0 + \delta f, \quad f_0 = \frac{n_e}{(2\pi T_e/m_e)^{3/2}} e^{-\frac{m_e w^2}{2T_e}} \quad (250)$$

5.1.2 1st order.

$$\int d\vec{w} \left(\frac{\partial \delta f}{\partial \vec{v}} \right)_{w_{\perp}, w_{\parallel}} + 2D \mathcal{L} [f_0 + \delta f] + \left(\frac{\partial \delta f}{\partial t} \right)_{e,e} = \text{frame difference}$$

\swarrow 0 to lowest order, but not to 1st because of the frame difference

$$f_0 = \frac{n_e}{(\pi v_{the}^2)^{3/2}} e^{-\frac{m_e (\vec{w}' + \vec{u}_i - \vec{u}_e)^2}{2T_e}}$$

$$\approx f_0(w') + (\vec{u}_i - \vec{u}_e) \cdot \left(\frac{\partial f_0}{\partial \vec{w}} \right)$$

\uparrow
 annihilated by \mathcal{L}
 $\vec{w}' = \vec{v} - \vec{u}_i$

$$- \frac{2\vec{w} \cdot (\vec{u}_i - \vec{u}_e)}{v_{the}^2} f_0$$

$$\mathcal{L} \left[- \frac{2\vec{w} \cdot (\vec{u}_i - \vec{u}_e)}{v_{the}^2} f_0 \right]$$

$$= \frac{2\vec{w} \cdot (\vec{u}_i - \vec{u}_e)}{v_{the}^2} f_0 \text{ because}$$

$$\mathcal{L}[\vec{w}] = -\vec{w}$$

$$\begin{aligned}
 &= \vec{w} \cdot \nabla f_0 + \vec{a}_e \cdot \frac{\partial f_0}{\partial \vec{w}} = \vec{w} \cdot \left[\frac{\nabla n_e}{n_e} - \frac{3}{2} \frac{\nabla T_e}{T_e} + \frac{w^2}{v_{the}^2} \frac{\nabla T_e}{T_e} \right] f_0 \\
 &\quad - \frac{\nabla P_e - \vec{R}_{ei}}{m_e n_e} \cdot \frac{m_e}{T_e} \vec{w} f_0 \\
 &= \vec{w} \cdot \left[\cancel{\frac{\nabla P_e}{P_e}} + \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) \frac{\nabla T_e}{T_e} \right. \\
 &\quad \left. - \cancel{\frac{\nabla P_e}{P_e}} + \frac{\vec{R}_{ei}}{P_e} \right] f_0 \quad (251)
 \end{aligned}$$

$\nabla P_e - \vec{R}_{ei}$
 $m_e n_e$
 to lowest order,
 pressure of the f_0 is
 isotropic

\vec{R}_{ei} itself depends on δf : let's work this out.

By definition,

$$\vec{R}_{ei} = \int d\vec{w}' m_e \vec{w}' \left(\frac{\partial f_e}{\partial t} \right)_{c,i} = \int d\vec{w}' m_e \vec{w}' \nu_D(w') \mathcal{L}[f_e]$$

$$= -m_e \int d\vec{w}' \nu_D(w') \vec{w}' f_e \quad \text{because } \mathcal{L}[\vec{w}'] = -\vec{w}'$$

\uparrow but this function is a function of $\vec{w} = \vec{v} - \vec{u}_e = \vec{w}' + \vec{u}_i - \vec{u}_e$

$$= -m_e \int d\vec{w}' \nu_D(w') \vec{w}' \left[f_e(\vec{w}') + (\vec{u}_i - \vec{u}_e) \cdot \frac{\partial f_e}{\partial \vec{w}'} \right]$$

\downarrow $f_0(\vec{w}') + \delta f(\vec{w}')$ ← same order
 \downarrow Vanishes under integration

$$= -m_e \int d\vec{w}' \nu_D(w') \vec{w}' \delta f(\vec{w}')$$

$$+ \frac{2m_e}{v_{the}^2} \int d\vec{w}' \nu_D(w') \vec{w}' \vec{w}' \cdot (\vec{u}_i - \vec{u}_e) \quad (252)$$

\downarrow
 $-m_e n_e \nu_{ei} (\vec{u}_e - \vec{u}_i)$ friction force for a Maxwellian previously calculated!

OK, let us assemble everything:

$$\Sigma_e \left(\frac{\partial \delta f}{\partial t} \right)_{w_{\perp}, w_{\parallel}} + \frac{2\vec{w} \cdot (\vec{u}_i - \vec{u}_e)}{v_{the}^2} v_D(w) f_0 + v_D(w) \mathcal{L}[\delta f]$$

$$+ \left(\frac{\partial \delta f}{\partial t} \right)_{c,e} = \vec{w} \cdot \left[\frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) - \frac{m_e}{T_e} v_{ei} (\vec{u}_e - \vec{u}_i) - \frac{m_e}{Pe} \int d\vec{w}' v_D(w') \vec{w}' \delta f(\vec{w}') \right] f_0$$

$$\Sigma_e \frac{\partial \delta f}{\partial t} + \underbrace{v_D(w) \mathcal{L}[\delta f] + \frac{2f_0}{ne v_{the}^2} \vec{w} \cdot \int d\vec{w}' v_D(w') \vec{w}' \delta f(\vec{w}')}_{\text{modified Lorentz operator}}$$

$$+ \left(\frac{\partial \delta f}{\partial t} \right)_{c,e} = \vec{w} \cdot \left\{ \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) - \frac{2}{v_{the}^2} [v_{ei} - v_D(w)] (\vec{u}_e - \vec{u}_i) \right\} \quad (253)$$

→ This "modified" Lorentz operator is a rather marvellous thing: it scatters particles but makes sure to conserve their momentum, so that δf does not develop a mean \vec{w} - which it is not allowed to do by definition of \vec{w} ! Indeed:

$$\begin{aligned} & \int d\vec{w} \vec{w} \left[v_D(w) \mathcal{L}[\delta f] + \frac{2f_0}{ne v_{the}^2} \vec{w} \cdot \int d\vec{w}' v_D(w') \vec{w}' \delta f(\vec{w}') \right] \\ &= - \int d\vec{w} v_D(w) \vec{w} \delta f + \underbrace{\left(\int d\vec{w} \frac{2f_0}{ne v_{the}^2} \vec{w} \vec{w} \right)}_{\text{momentum conservation}} \cdot \int d\vec{w}' v_D(w') \vec{w}' \delta f(\vec{w}') \\ &= 0, \text{ q.e.d.} \quad \frac{2}{3} \frac{1}{ne v_{the}^2} \int d\vec{w} w^2 f_0 = 1 \end{aligned}$$

OK, now, to solve (253), we separate the gyrotopic and gyroangle-dependent parts:

$$\delta f = \langle \delta f \rangle_{\theta} + \delta \tilde{f} \quad (254)$$

W/o the ~~the~~ e-e collisions, (256) becomes

$$\begin{aligned} \frac{1}{2} \frac{\partial}{\partial \zeta} (1 - \zeta^2) \frac{\partial \langle \delta f \rangle}{\partial \zeta} + \frac{4\pi W^4 f_0(W)}{n_e v_{the}^2} &\approx \int_0^\infty d\omega' \int_{-1}^1 d\zeta' \zeta' \langle \delta f \rangle \\ &= \approx \frac{W f_0(W)}{v_D(W)} \uparrow \cdot \left\{ \frac{\partial T_e}{T_e} \left(\frac{W^2}{v_{the}^2} - \frac{5}{2} \right) - \frac{2 [v_{ei} - v_D(W)]}{v_{the}^2} (\bar{u}_e - \bar{u}_i) \right\} \\ &\equiv \approx C(W) \quad (257) \end{aligned}$$

Let us look for a solution in the form (obviously)

$$\langle \delta f \rangle = \approx h(\omega) \quad (258)$$

$$-h(\omega) + \frac{8\pi W^4 f_0(\omega)}{3 n_e v_{the}^2} \int_0^\infty d\omega' h(\omega') = C(\omega) \quad (259)$$

Note that both sides of this equation integrate to 0:

$$\frac{8\pi}{3 n_e v_{the}^2} \int_0^\infty d\omega W^4 f_0(\omega) = \frac{8\pi}{3\sqrt{\pi}} \int_0^\infty dx x^4 e^{-x^2} = 1 \quad (260)$$

$\underbrace{\hspace{10em}}_{\frac{1}{2} \cdot \frac{3}{2} \cdot \frac{\sqrt{\pi}}{2}}$

$$\int_0^\infty d\omega C(\omega) = \int_0^\infty d\omega \frac{W f_0(\omega)}{v_D(\omega)} \uparrow \cdot \left\{ \frac{\partial T_e}{T_e} \left(\frac{W^2}{v_{the}^2} - \frac{5}{2} \right) - \frac{2 [v_{ei} - v_D(\omega)]}{v_{the}^2} (\bar{u}_e - \bar{u}_i) \right\} \quad (261)$$

$\textcircled{1} \qquad \qquad \qquad \textcircled{2}$

$$\textcircled{1} \propto \int_0^\infty d\omega W^4 f_0(\omega) \left(\frac{W^2}{v_{the}^2} - \frac{5}{2} \right) \propto \int_0^\infty dx e^{-x^2} x^4 \left(x^2 - \frac{5}{2} \right) = 0$$

$$\textcircled{2} \propto \int_0^\infty d\omega W f_0(\omega) \left[\frac{v_{ei}}{v_D(\omega)} - 1 \right] \propto \int_0^\infty dx x e^{-x^2} \left(\frac{4}{3\sqrt{\pi}} x^3 - 1 \right) = \frac{1}{2} - \frac{1}{2} = 0$$

Recall that

$$v_D(\omega) = \frac{4\pi Z e^4 n_e \lambda_{ei}}{m_e^2 \omega^3} \quad \Rightarrow \quad \frac{v_D}{v_{ei}} = \frac{4\pi}{m_e^2 \omega^3} \frac{m_e^{1/2} T_e^{3/2}}{4\sqrt{2\pi}} \cdot 3$$

$$v_{ei} = \frac{4\sqrt{2\pi}}{3} \frac{Z e^4 n_e \lambda_{ei}}{m_e^{1/2} T_e^{3/2}} \quad \Rightarrow \quad = 3 \sqrt{\frac{\pi}{2}} \left(\frac{v_{the}}{\sqrt{2} W} \right)^3 = \frac{3\sqrt{\pi}}{4} \left(\frac{v_{the}}{W} \right)^3 \quad (262)$$

-115a-

~~W~~ This means that

$$h(w) = -C(w) \quad (263)$$

is perfectly good particular solution. But there is also a homogeneous solution:

$$h_{\text{hom}}(w) = \frac{8\pi W^4 f_0(w)}{3n_e v_{the}^2} \alpha, \quad (264)$$

where the constant α is determined from the requirement that $\int d\vec{w} w_{||} \langle of \rangle = 0$. Let us implement this:

$$\begin{aligned} \int d\vec{w} w_{||} \approx h_{\text{hom}}(w) &= \alpha \int dW W^3 \frac{4\pi}{3} \frac{8\pi W^4 f_0(w)}{3n_e v_{the}^2} = \\ &= \frac{32\pi^2}{9} \alpha \int_0^\infty dW W^7 \frac{e^{-W^2/v_{the}^2}}{\pi^{3/2} v_{the}^5} = \frac{32\sqrt{\pi}}{9} \alpha v_{the}^3 \underbrace{\int_0^\infty dx x^7 e^{-x^2}}_{\int_0^\infty dy y^3 e^{-y} = 3} \\ &= \frac{32\sqrt{\pi}}{3} \alpha v_{the}^3 \end{aligned} \quad (264a)$$

$$\int d\vec{w} w_{||} \approx C(w) = \frac{4\pi}{3} \int_0^\infty dW W^3 \frac{W f_0(w)}{v_D(w)} \uparrow \cdot \{ \dots \} \quad \uparrow \text{see (257)}$$

$$= \frac{4\pi}{3} \frac{1}{W^3 v_D(w)} \int_0^\infty dW W^7 f_0(w) \uparrow \cdot \left\{ \frac{\nabla T_e}{T_e} \left(\frac{W^2}{v_{the}^2} - \frac{5}{2} \right) - \right.$$

\uparrow const!

$$\left. - \frac{2v_{ei}}{v_{the}^2} \left[1 - \frac{3\sqrt{\pi}}{4} \left(\frac{v_{the}}{W} \right)^3 \right] (\vec{u}_e - \vec{u}_i) \right\}$$

$$= \frac{4\pi}{3} \frac{n_e v_{the}^5}{\pi^{3/2} W^3 v_D(w)} \int_0^\infty dx x^7 e^{-x^2} \uparrow \cdot \left\{ \frac{\nabla T_e}{T_e} \left(x^2 - \frac{5}{2} \right) - \right.$$

$$\left. - \frac{2v_{ei}}{v_{the}^2} \left(1 - \frac{3\sqrt{\pi}}{4} \frac{1}{x^3} \right) (\vec{u}_e - \vec{u}_i) \right\}$$

$$= \frac{4}{3\sqrt{\pi}} \frac{n_e v_{the}^5}{W^3 v_D} \uparrow \cdot \left\{ \frac{\nabla T_e}{T_e} \frac{1}{2} (4! - \frac{5}{2} \cdot 3!) - \frac{2v_{ei}}{v_{the}^2} (\vec{u}_e - \vec{u}_i) \left(\frac{1}{2} \cdot 3! - \frac{3\sqrt{\pi}}{4} \frac{3\sqrt{\pi}}{8} \right) \right\}$$

$$= \frac{4}{\sqrt{\pi}} \frac{n_e v_{the}^5}{W^3 v_D} \uparrow \cdot \left\{ \frac{3}{2} \frac{\nabla T_e}{T_e} - \frac{2v_{ei}}{v_{the}^2} (\vec{u}_e - \vec{u}_i) \left(1 - \frac{3\sqrt{\pi}}{32} \right) \right\} \quad (264b)$$

Requiring that this be cancelled by α gives

$$\alpha = \frac{3}{8\pi} \frac{n_e v_{the}^2}{\omega^3 v_D} \hat{b} \cdot \{ \dots \} \Rightarrow h_{hom}(\omega) = \frac{\omega f_0(\omega)}{v_D(\omega)} \hat{b} \cdot \{ \dots \}$$

Assembling terms,

$$\langle sf \rangle = - \frac{\omega_{||} f_0(\omega)}{v_D(\omega)} \hat{b} \cdot \left\{ \frac{\nabla T_e}{T_e} \left(\frac{\omega^2}{v_{the}^2} - 4 \right) - \frac{2v_{ei}}{v_{the}^2} \left[\frac{3\pi}{32} - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{\omega^3} \right] (\vec{u}_e - \vec{u}_i) \right\}$$

(265)

5.1.4 Parallel friction force

Let us not delay at least some gratification and see how this result allows us to amend our previous calculation of the e-i friction force. Its definition is (252) and from $\langle sf \rangle$ we can now calculate its $||$ component ($\langle sf \rangle$'s contributions to \vec{R}_{jei} vanish):

$$R_{||ei} = -m_e n_e v_{ei} (u_{||e} - u_{||i}) - m_e \int d\vec{\omega} v_D(\omega) \vec{\omega}_{||} \langle sf \rangle$$

$$\begin{aligned} &\Rightarrow - \int d\vec{\omega} \omega_{||}^2 f_0(\omega) \hat{b} \cdot \{ \dots \} = - \int_0^\infty d\omega \omega^4 f_0(\omega) \frac{4\pi}{3} \hat{b} \cdot \{ \dots \} \\ &= - \frac{4\pi}{3} \frac{n_e v_{the}^2}{\pi^{3/2}} \int_0^\infty dx x^4 e^{-x^2} \hat{b} \cdot \left\{ \frac{\nabla T_e}{T_e} (x^2 - 4) - \frac{2v_{ei}}{v_{the}^2} \left(\frac{3\pi}{32} - \frac{3\sqrt{\pi}}{4} \frac{1}{x^3} \right) (\vec{u}_e - \vec{u}_i) \right\} \\ &= - \frac{4\pi}{3\sqrt{\pi}} n_e v_{the}^2 \left[\frac{\nabla_{||} T_e}{T_e} \frac{\sqrt{\pi}}{2} \frac{1}{2} \frac{3}{2} \left(\frac{5}{2} - 4 \right) - \frac{2v_{ei}}{v_{the}^2} \left(\frac{3\pi}{32} \cdot \frac{\sqrt{\pi}}{2} \frac{3}{4} - \frac{3\sqrt{\pi}}{4} \cdot \frac{1}{2} \right) (\vec{u}_e - \vec{u}_i) \right] \\ &= - \frac{4\pi}{3\sqrt{\pi}} n_e v_{the}^2 \left[- \frac{3}{4} \frac{\nabla_{||} T_e}{T_e} - \frac{v_{ei}}{v_{the}^2} \left(\frac{3\pi}{32} - 1 \right) (\vec{u}_e - \vec{u}_i) \right] \end{aligned}$$

$$= + \frac{n_e}{m_e} \frac{3}{2} \nabla_{||} T_e + n_e v_{ei} \left(\frac{3\pi}{32} - 1 \right) (\vec{u}_e - \vec{u}_i)$$

Thus,

$$R_{\parallel e i} = -\frac{3\pi}{32} m_e n_e v_{ei} (u_{\parallel e} - u_{\parallel i}) - \frac{3}{2} n_e \nabla_{\parallel} T_e \quad (266)$$

This is the familiar Spitzer-Hairou result. In the $Z=1$ correct calculation, the coeff. becomes 0.51

This bit is a new feature. In the $Z=1$ case, the coeff. is 0.71

The physics of the new term is this: electrons coming from low temperatures collide more often and so lose more momentum than those from high temperatures. The result is net friction between them.

This is called the "thermoelectric effect": put this back into (243) and discover that collisions lead to a contribution to parallel current - I will discuss this in § 5.2.

5.1.5 Non-gyrotropic part of δf

Let us now subtract (256) from (253):

$$\begin{aligned} \Omega_e \frac{\partial \delta \tilde{f}}{\partial t} + v_D(w) \mathcal{L}[\delta \tilde{f}] + \frac{2 f_0(w)}{n_e v_{the}^2} \bar{w}_L \cdot \int d\tilde{w}' v_D(w') \bar{w}'_L \delta \tilde{f}(\tilde{w}') \\ + \left(\frac{\partial \delta \tilde{f}}{\partial t} \right)_{c,e} = \bar{w}_L \cdot \left\{ \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) - \frac{2 v_{ei}}{v_{the}^2} \left[1 - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{w^3} \right] (\bar{u}_e - \bar{u}_i) \right\} f_0(w) \end{aligned} \quad (267)$$

I am going to solve this in the subsidiary expansion

$$\frac{v_{ei}}{\Omega_e} \ll 1 \text{ — but still } \gg \sqrt{\frac{m_e}{m_i}} \sim k \rho_e$$

$$\delta \tilde{f} = \delta \tilde{f}^{(0)} + \delta \tilde{f}^{(1)} \quad (268)$$

This means that to lowest order, I can just drop all collisional terms:

$$\Omega_e \frac{\partial \delta \tilde{f}^{(0)}}{\partial t} = \vec{w}_L \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) f_0(w) \quad (269)$$

$$\hookrightarrow = \frac{\partial}{\partial \vartheta} \vec{w}_L \times \hat{b} \text{ — check this by letting } \vec{w}_L = w_L (\hat{x} \cos \vartheta + \hat{y} \sin \vartheta)$$

So, solution:

$$\delta \tilde{f}^{(0)} = \frac{\vec{w}_L \times \hat{b}}{\Omega_e} \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) f_0(w) \quad (270)$$

This part of δf is entirely independent of collisions, it is an FLR effect!

To get something collisional, let us go to next order:

$$\Omega_e \frac{\partial \delta \tilde{f}^{(1)}}{\partial t} = -\nu_D(w) \mathcal{L} [\delta \tilde{f}^{(0)}] - \frac{2 f_0(w)}{n_e v_{the}} \vec{w}_L \cdot \int d\vec{w}' \nu_D(w') \vec{w}'_L \delta \tilde{f}^{(0)}(\vec{w}') - \left(\frac{\partial \delta \tilde{f}^{(0)}}{\partial t} \right)_{c,e} - \frac{2 v_{ei}}{v_{the}^2} \left[1 - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{w^3} \right] \vec{w}_L \cdot (\vec{u}_e - \vec{u}_i) f_0(w) \quad (271)$$

~~It is not hard to see that $\mathcal{L}[\vec{w}_*] = -\vec{w}_*$, so~~

It is not hard to see that $\mathcal{L}[\vec{w}_*] = -\vec{w}_*$, so

$$\mathcal{L}[\delta \tilde{f}^{(0)}] = -\delta \tilde{f}^{(0)} \quad (272)$$

Note that $\int d\vec{w} \vec{w} \delta \tilde{f}^{(0)} = 0$, so all is well.

$$\int d\vec{w} \nu_D(w) \vec{w}_\perp \delta f^{(0)} = \int d\vec{w} \nu_D(w) \vec{w}_\perp \frac{\vec{w}_\perp \times \hat{b}}{\Omega_e} \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) f_0(w)$$

$$= \left\{ \left[\int d\vec{w} \nu_D(w) \vec{w}_\perp \vec{w}_\perp \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) f_0 \right] \times \frac{\hat{b}}{\Omega_e} \right\} \cdot \frac{\nabla T_e}{T_e}$$

averaging this gives $(1 - \langle \hat{b} \hat{b} \rangle) \frac{w^2}{2} (1 - \frac{5}{2})$

$$= \int_0^\infty dw w^2 \frac{1}{2\pi} \int d\zeta (1 - \zeta^2) \frac{1}{2} \nu_D(w) w^2 \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) f_0 \frac{\hat{b}}{\Omega_e} \times \frac{\nabla T_e}{T_e}$$

$$= \frac{4\pi}{3} \int_0^\infty dw w^4 \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) \nu_D(w) f_0 \frac{\hat{b} \times \nabla T_e}{\Omega_e T_e} =$$

$$\frac{vei \pi^{3/2} v_{the}}{T^{3/2} v_{the}^3} \int_0^\infty dw w \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) \frac{\beta \sqrt{\pi} v_{the}^3}{4 w^3} vei e^{-w^2/v_{the}^2}$$

$$= \frac{\hat{b} \times \nabla T_e}{\Omega_e} \frac{vei n_e}{me} \int_0^\infty dx (x - \frac{5}{2}) e^{-x} = -\frac{3}{2} \frac{ne vei}{me} \frac{\hat{b} \times \nabla T_e}{\Omega_e} \quad (273)$$

Thus,

$$\Omega_e \frac{\partial \delta f^{(1)}}{\partial t} = \nu_D(w) \delta f^{(0)} \left[\text{crossed out terms} \right] - \left(\frac{\partial \delta f^{(0)}}{\partial t} \right)_{ge}$$

$$+ \frac{2f_0}{v_{the}} vei \vec{w}_\perp \cdot \left[\frac{3}{2me} \frac{\hat{b} \times \nabla T_e}{\Omega_e} - \left(1 - \frac{3\sqrt{\pi} v_{th}^3}{4 w^3} \right) (\vec{u}_e - \vec{u}_i) \right]$$

(274)

I will yet again ignore e-e collisions and integrate

using $\vec{w}_\perp = \frac{\partial}{\partial \theta} \vec{w}_\perp \times \hat{b}$, $\vec{w}_\perp \times \hat{b} = -\frac{\partial \vec{w}_\perp}{\partial \theta}$

$$\delta f^{(1)} = -\frac{\nu_D(w)}{\Omega_e^2} \vec{w}_\perp \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{th}^2} - \frac{5}{2} \right) f_0 + \frac{vei}{\Omega_e} (\vec{w}_\perp \times \hat{b}) \cdot \left[\frac{3}{2} \frac{\hat{b} \times \nabla T_e}{\Omega_e T_e} - \left(1 - \frac{3\sqrt{\pi} v_{th}^3}{4 w^3} \right) \frac{2}{v_{the}^2} (\vec{u}_e - \vec{u}_i) \right] f_0 \quad (275)$$

Ex. Check to see if this has an unphysical flow!

5.1.6 Perpendicular friction force

I have in fact already computed this. By definition,

$$\vec{R}_{ei\perp}^{(1)} = -m_e n_e v_{ei} (\vec{u}_e - \vec{u}_i)_\perp - m_e \int d\vec{w} v_D(w) \vec{w}_\perp \delta f^{(1)}(\vec{w})$$

$$\vec{R}_{ei\perp}^{(1)} = -m_e n_e v_{ei} (\vec{u}_e - \vec{u}_i)_\perp + \frac{3}{2} n_e v_{ei} \frac{\vec{b} \times \nabla T_e}{\Omega_e} \quad (276)$$

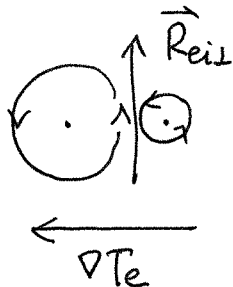
\uparrow
 $\Omega_e < 0$

"

$$-\frac{3}{2} \frac{n_e v_{ei}}{m_e} \frac{\vec{b} \times \nabla T_e}{\Omega_e}$$

from (273)

The physics of the ∇T_e contribution is similar to the physics of the $\nabla_{\parallel} T_e$ one:



Gyrating particles on the colder side have smaller velocities, so collide more than the ones on the hotter side. The result is net friction in the direction $\vec{b} \times \nabla T_e$.

There is no great point in calculating the contribution from $\delta f^{(1)}$, which are 2-nd order in v_{ei}/Ω_e , $\vec{R}_{ei\perp}^{(2)}$, but be my guest and explore them!

It will be more interesting to use our δf to work out the electron heat flux.

P.S. Here is a slightly faster way of getting δf (due to Helander & Sigmar).

Write eq. (253), neglecting e-e collisions, in the following form:

$$\Omega_e \frac{\partial \delta f}{\partial t} + \nu_D(w) \mathcal{L}[\delta f] + \vec{w} \cdot \vec{U}[\delta f] = \vec{w} \cdot \vec{G}(w) \quad (277)$$

Seek solution in the form ↑ short notation for corresponding terms

$$\delta f = \vec{w} \cdot \vec{F}(w) \quad (278)$$

Since $\frac{\partial \vec{w}}{\partial t} = -\vec{w}_\perp \times \hat{b}$ and $\mathcal{L}[\vec{w}] = -\vec{w}$, we get

$$-\Omega_e (\vec{w}_\perp \times \hat{b}) \cdot \vec{F} - \nu_D(w) \vec{w} \cdot \vec{F} + \vec{w} \cdot \vec{U}[\vec{w} \cdot \vec{F}] = \vec{w} \cdot \vec{G} \quad (279)$$

Since this must be satisfied $\forall \vec{w}$, we have

$$-\Omega_e \hat{b} \times \vec{F} - \nu_D \vec{F} + \vec{U}[\vec{w} \cdot \vec{F}] = \vec{G} \quad (280)$$

Note that

$$\begin{aligned} \vec{U}[\vec{w} \cdot \vec{F}] &= \frac{2f_0}{n_e v_{the}^2} \int d\vec{w}' \nu_D(w') \vec{w}' \vec{w}' \cdot \vec{F}(w') \\ &= \frac{8\pi f_0}{3n_e v_{the}^2} \int_0^\infty dw' w'^4 \nu_D(w') \vec{F}(w') \\ &= \frac{8\pi f_0 w^3 \nu_D(w)}{3n_e v_{the}^2} \int_0^\infty dw' w' \vec{F}(w') \equiv \nu_D \vec{V}[\vec{F}] \quad (281) \end{aligned}$$

$$-\Omega_e \hat{b} \times \vec{F} - \nu_D (\vec{F} - \vec{V}[\vec{F}]) = \vec{G} \quad (282)$$

Taking the parallel component gives the gyroviscous part of the distribution:

$$F_{||} - V_{||}[F_{||}] = -\frac{G_{||}}{\nu_D} \quad (283)$$

$$\boxed{F_{||} = -\frac{G_{||}}{\nu_D}} \text{ because } V_{||}\left[\frac{G_{||}}{\nu_D}\right] = 0 \quad (284)$$

This has to be adjusted by adding the homogeneous solution $(F_{||hom} = \alpha(\dots))$ on their calculation α to ensure $\int d\vec{w} w_{||} \delta f = 0$ - same way I did it above. The function α of $G_{||}$ adjusts accordingly.

Now take (282)_L:

$$\Omega_e \hat{b} \times \vec{F}_L + \nu_D (\vec{F}_L - \vec{V}_L(\vec{F}_L)) = -\vec{G}_L \quad (285)$$

To 0th order in ν_D/Ω_e ,

$$\hat{b} \times | \Omega_e \hat{b} \times \vec{F}_L^{(0)} = -\vec{G}_L \Rightarrow \boxed{\vec{F}_L^{(0)} = \frac{\hat{b} \times \vec{G}_L}{\Omega_e}} \quad (286)$$

To 1st order,

$$\hat{b} \times | \Omega_e \hat{b} \times \vec{F}_L^{(1)} = -\nu_D [\vec{F}_L^{(0)} - \vec{V}_L(\vec{F}_L^{(0)})] \quad (287)$$

$$\vec{F}_L^{(1)} = \frac{\nu_D}{\Omega_e} [\hat{b} \times \vec{F}_L^{(0)} - \vec{V}_L(\hat{b} \times \vec{F}_L^{(0)})]$$

$$\boxed{\vec{F}_L^{(1)} = -\frac{\nu_D}{\Omega_e} \left[\frac{\vec{G}_L}{\Omega_e} - \vec{V}_L\left(\frac{\vec{G}_L}{\Omega_e}\right) \right]} \quad (288)$$

adjusted with hom. solution.

Assembly (284), (286) and (288) via (278),

$$\delta f = - \left[\frac{w_{\parallel} \hat{G}_{\parallel}}{\nu_D} + \left[\frac{\vec{w}_L \times \hat{b}}{\Omega_e} + \vec{w}_L \frac{\nu_D}{\Omega_e^2} \right] \cdot \vec{G}_L + \frac{\nu_D}{\Omega_e^2} \vec{w}_L \cdot \vec{V}_L(\vec{G}_L) \right], \quad (289)$$

which is the same solution as previously calculated.

This is a neater way to do it, perhaps.

Note that where \vec{G} is multiplied ν_D/Ω_e^2 , the $\vec{u}_e - \vec{u}_i$ term in it can be dropped.

Note that Helander's treatment of "Lorentz plasma" (his §4.2) is probably the shortest possible treatment of the material I am presenting here - shorter than mine because he does not go to \vec{w} variables - but I wanted to preserve unity with KMHD treatment and some later convenience.

5.2 Generalised Ohm's Law

To lowest order in our expansion,

$$\vec{E} + \frac{\vec{u}_e \times \vec{B}}{c} = -\frac{\nabla p_e}{e n_e} + \frac{\vec{R}_{ei}}{e n_e} \quad (290)$$

So resistivity in a magnetised plasma is anisotropic, but not by much. In any event, we can neglect $j_{\perp} \ll j_{\parallel}$ because we know from KMHD that $\vec{u}_{Te} \approx \vec{u}_{Ti}$ to lowest order in k_{\perp} .

$$\left\{ \begin{aligned} & - \frac{3\pi}{32} \frac{m_e v_{ei}}{e^2 n_e} n_e (u_{\parallel e} - u_{\parallel i}) \hat{b} \\ & - \frac{n_e v_{ei}}{e^2 n_e} n_e (\vec{u}_{\perp e} - \vec{u}_{\perp i}) \\ & - \frac{3}{2} \frac{\nabla_{\parallel} T_e}{e} \hat{b} + \frac{3}{2} \frac{v_{ei}}{e n_e} \hat{b} \times \nabla T_e \end{aligned} \right.$$

η_{\parallel} η_{\perp} "Seebeck effect" "Nernst effect"

We can treat (290) as an equation for \parallel current:

$$j_{\parallel} = \frac{1}{\eta_{\parallel}} E_{\parallel} + \frac{32}{3\pi} \frac{e}{m_e v_{ei}} (\nabla_{\parallel} p_e + \frac{3}{2} n_e \nabla_{\parallel} T_e) \quad (291)$$

$\underbrace{\hspace{10em}}_{\text{Ohm}} \quad \underbrace{\hspace{10em}}_{\text{collisionless}} \quad \underbrace{\hspace{10em}}_{\text{collisional (Seebeck)}} \quad \underbrace{\hspace{10em}}_{\text{thermoelectric effect (gradient drive currents)}}$

We can also just recall that $\vec{j} = \frac{c}{4\pi} \nabla \times \vec{B}$ and treat (290) as the equation for the electric field to be put into the Faraday's Law

$$\frac{\partial \vec{B}}{\partial t} = -c \nabla \times \vec{E} = \nabla \times \left(\vec{u}_e \times \vec{B} + c \frac{\nabla p_e}{e n_e} - c \frac{\vec{R}_{ei}}{e n_e} \right)$$

$$= \nabla \times (\vec{u}_e \times \vec{B}) - \frac{c}{e n_e} \nabla n_e \times \nabla T_e - \nabla \times c \frac{\vec{R}_{ei}}{e n_e} \quad (292)$$

produces, rather than merely amplifies fields \rightsquigarrow "Biermann battery"

Believed responsible for primordial magnetic fields seen in the LSS for the first time by G. Gregori.

5.3 Electron ~~Energy Balance~~

5.3.1 Electron temperature eqn.

Let us now talk about flows of energy.

From $\int d\vec{w} \frac{m_e w^2}{2}$ (240), we get, in full generality

$$\frac{d}{dt} \frac{3}{2} P_e + \int d\vec{w} \frac{m_e w^2}{2} \vec{w} \cdot \nabla f_e \quad \text{---} \quad -m_e \bar{a}_e \int d\vec{w} \vec{w} f_e = 0$$

$$\frac{3}{2} n_e \frac{dT_e}{dt}$$

$\nabla \cdot \vec{q}_e$ heat flux

$$+ \frac{3}{2} T_e \frac{dn_e}{dt}$$

$$+ \int d\vec{w} \frac{m_e w^2}{2} \left(-\frac{e}{m_e} \frac{\vec{w} \times \vec{B}}{c} - \vec{w} \cdot \nabla \vec{u}_e + \vec{g}_e \right) \cdot \frac{\partial f_e}{\partial \vec{w}} =$$

$$-\frac{3}{2} P_e \nabla \cdot \vec{u}_e$$

$$m_e \int d\vec{w} f_e (\vec{w} \vec{w} : \nabla \vec{u}_e + \frac{w^2}{2} \nabla \cdot \vec{u}_e) = \frac{3}{2} P_e \nabla \cdot \vec{u}_e + \hat{P}_e : \nabla \vec{u}_e$$

// $\nabla \cdot \vec{q}_e$ heat flux

// cons. of energy

// $\vec{u}_e \cdot \vec{R}_{ei}$

$P_{e\parallel} + \hat{P}_e$
↑ small (el. viscosity)

$$= \int d\vec{w} \frac{m_e w^2}{2} \left(\frac{\partial f_e}{\partial t} \right)_c = \int d\vec{v} \frac{m_e}{2} (v^2 - 2\vec{v} \cdot \vec{u}_e + \frac{u_e^2}{2}) \left(\frac{\partial f_e}{\partial t} \right)_c$$

$$= \int d\vec{v} \frac{m_e v^2}{2} \left(\frac{\partial f_e}{\partial t} \right)_c - m_e \vec{u}_e \cdot \int d\vec{v} \vec{v} \left(\frac{\partial f_e}{\partial t} \right)_c$$

$$- \int d\vec{v} \frac{m_e v^2}{2} \left(\frac{\partial f_i}{\partial t} \right)_c = \vec{R}_{ei} \cdot \vec{u}_i + 3 n_i v_{ie} (T_i - T_e)$$

$$= + \vec{R}_{ei} \cdot (\vec{u}_i - \vec{u}_e) - 3 \frac{m_e}{m_i} n_e v_{ei} (T_e - T_i) \quad (296)$$

this is very small in our expansion

Ohmic heating etc: $\eta_{\parallel} j_{\parallel}^2 + \dots$

So, we have

$$\frac{3}{2} n_e \frac{dT_e}{dt} + \nabla \cdot \vec{q}_e + p_e \nabla \cdot \vec{u}_e + \hat{\Pi}_e : \nabla \vec{u}_e = \frac{R_{ei}}{e n_e} \cdot \vec{j} - 3 \frac{m_e}{m_i} n_e v_{ei} (T_e - T_i)$$

↑
compressional heating
(adiabatic effect)
↑
electron viscosity
↑
electric heating
↑
temperature relaxation

our focus here will be the e. heat flux

$$\vec{q}_e = \int d\vec{w} \frac{m_e w^2}{2} \vec{w} f_e \quad (298)$$

To calculate it, all we need to do is substitute our δf (no heat flux in the Maxwellian f_0).

5.3.2 Parallel heat flux

From (265),

$$q_{\parallel e} = - \int d\vec{w} \frac{m_e w^2}{2} w_{\parallel}^2 \frac{f_0(w)}{v_D(w)} \left\{ \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - 4 \right) - \frac{2v_{ei}}{v_{the}^2} \left(\frac{3\pi}{32} - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{w^3} \right) (\vec{u}_e - \vec{u}_i) \right\}$$

$\frac{n_e}{\pi^{3/2} v_{the}^3} e^{-w^2/v_{the}^2}$

$m_e 2\pi \frac{1}{2} \int_0^{\infty} dw w^6 \cdot \frac{2}{3}$
 $\frac{3\sqrt{\pi}}{4} v_{ei} \frac{v_{the}^3}{w^3}$

$$= - \frac{m_e n_e v_{the}^4}{v_{ei}} \frac{8}{9\pi} \int_0^{\infty} dx x^9 e^{-x^2} \left[\frac{\nabla_{\parallel} T_e}{T_e} (x^2 - 4) - \frac{2v_{ei}}{v_{the}^2} \left(\frac{3\pi}{32} - \frac{3\sqrt{\pi}}{4x^3} \right) (\vec{u}_e - \vec{u}_i) \right]$$

$$= - \frac{n_e v_{the}^2}{v_{ei}} \frac{16}{9\pi} \nabla_{\parallel} T_e \frac{1}{2} \int_0^{\infty} dy y^4 e^{-y} (y-4) \quad \left(\frac{\sqrt{\pi}}{2} \frac{1}{2} \cdot \frac{3}{2} \cdot \frac{5}{2} \right)$$

"4!"

$$+ m_e n_e v_{the}^2 \frac{16}{9\pi} (u_{\parallel e} - u_{\parallel i}) \left[\frac{3\pi}{32} \cdot \frac{4!}{2} - \frac{3\sqrt{\pi}}{4} \int_0^{\infty} dx x^6 e^{-x^2} \right]$$

$$= - \frac{64}{3\pi} \frac{n_e v_{the}^2}{v_{ei}} \nabla_{\parallel} T_e + \frac{3}{4} m_e n_e v_{the}^2 (u_{\parallel e} - u_{\parallel i}) \quad (299)$$

$$\text{So, } \left[q_{||e} = - \underbrace{\frac{128}{3\pi} \frac{n_e T_e}{m_e v_{the}}}_{\text{heat conductivity}} \nabla_{||} T_e + \frac{3}{2} n_e T_e (u_{||e} - u_{||i}) \right] \quad (299)$$

Regular collisional diffusion
 $\sim n_e \frac{v_{the}^2}{v_{ei}} \sim n_e v_{the} \lambda_{dp}$

\parallel heat conductivity $\equiv \kappa_{||}$
 At $Z=1$, the correct coefficients are 3.16 and 0.71
 $-\frac{3}{2} \frac{T_e}{e} j_{||}$ current carries heat
 "Peltier effect"

5.3.3 Diamagnetic heat flux

From (270),

$$q_{xe} = \int d\vec{w} \frac{m_e w^2}{2} \vec{w}_{\perp} \cdot \vec{f}^{(b)} = \int d\vec{w} \frac{m_e w^2}{2} \vec{w}_{\perp} \frac{\vec{w}_{\perp} \times \hat{b}}{\Omega_e} \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right)$$

$$= \left[\int d\vec{w} \frac{m_e w^2}{2} f_0(w) \vec{w}_{\perp} \vec{w}_{\perp} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) \right] \cdot \frac{\hat{b} \times \nabla T_e}{\Omega_e T_e}$$

$$\frac{m_e}{2} (1 - \hat{b}\hat{b})_{\perp} \frac{1}{Z} 2\pi \int d^3z (1 - z^2) \int d\vec{w} w^6 \frac{n_e}{\pi^{3/2} v_{the}^3} e^{-w^2/v_{the}^2} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right)$$

$$= m_e n_e v_{the}^4 (1 - \hat{b}\hat{b})_{\perp} \frac{2}{3\sqrt{\pi}} \int_0^{\infty} dx x^6 e^{-x^2} (x^2 - \frac{5}{2}) = \frac{5}{8} m_e n_e v_{the}^4 (1 - \hat{b}\hat{b})_{\perp}$$

$$\frac{\sqrt{\pi}}{2} \frac{1}{2} \cdot \frac{2}{2} \cdot \frac{5}{2} \left(\frac{7}{2} - \frac{5}{2} \right)$$

$$\boxed{q_{xe} = \frac{5}{8} \frac{n_e T_e}{m_e \Omega_e} \hat{b} \times \nabla T_e} \quad (300)$$

Physics of this is the same as of the \perp friction (276)

$\Omega_e \tau_e < 0!$ This is sometimes called Righi-Leduc effect (or thermal Hall effect)

5.3.4 Perpendicular Heat Flux

From (275),

$$\begin{aligned} \vec{q}_{\perp e} &= \int d\vec{w} \frac{m_e w^2}{2} \vec{w}_{\perp} \tilde{f}^{(1)} \\ &= + \int d\vec{w} \frac{m_e w^2}{2} \vec{w}_{\perp} \left\{ - \frac{v_D(w)}{\Omega_e^2} \vec{w}_{\perp} \cdot \frac{\nabla T_e}{T_e} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) f_0(w) \right. \\ &\quad \left. + \frac{v_{ei}}{\Omega_e} (\vec{w}_{\perp} \times \hat{b}) \cdot \left[\frac{3}{2} \frac{\hat{b} \times \nabla T_e}{\Omega_e T_e} - \left(1 - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{w^3} \right) \frac{2}{v_{the}^2} (\vec{u}_e \times \vec{u}_i) \right] f_0 \right\} \end{aligned}$$

see p.127

$$= \left[\int d\vec{w} \frac{m_e w^2}{2} \vec{w}_{\perp} \vec{w}_{\perp} f_0(w) \right] \cdot \left\{ - \frac{v_D(w)}{\Omega_e^2} \left(\frac{w^2}{v_{the}^2} - \frac{5}{2} \right) \frac{\nabla T_e}{T_e} + \frac{v_{ei}}{\Omega_e} \left[\frac{3}{2} \frac{\hat{b} \times (\hat{b} \times \nabla T_e)}{\Omega_e T_e} + \left(1 - \frac{3\sqrt{\pi}}{4} \frac{v_{the}^3}{w^3} \right) \frac{2}{v_{the}^2} \frac{\hat{b} \times \vec{j}}{c n_e} \right] \right\}$$

$$\rightarrow m_e n_e v_{the}^4 (1 - \hat{b}\hat{b}) \frac{2}{3\sqrt{\pi}} \int_0^{\infty} dx x^6 e^{-x^2} \rightarrow \frac{3\sqrt{\pi}}{4} \frac{1}{2} \left(-\frac{1}{2} \right)$$

$$= m_e n_e v_{the}^4 \frac{2}{3\sqrt{\pi}} \left\{ - \int_0^{\infty} dx x^3 \left(x^2 - \frac{5}{2} \right) e^{-x^2} \frac{3\sqrt{\pi}}{4} \frac{v_{ei}}{\Omega_e^2} \frac{\nabla_{\perp} T_e}{T_e} \right.$$

$$\left. - \frac{3}{2} \int_0^{\infty} dx x^6 e^{-x^2} \frac{v_{ei}}{\Omega_e^2} \frac{\nabla_{\perp} T_e}{T_e} + \frac{2v_{ei}}{\Omega_e v_{the}^2 c n_e} (\hat{b} \times \vec{j}) \right.$$

$$\left. \frac{3\sqrt{\pi}}{2} \frac{1}{2} \frac{3 \cdot 5}{2 \cdot 2} \cdot \int_0^{\infty} dx x^6 e^{-x^2} \left(1 - \frac{3\sqrt{\pi}}{4} \frac{1}{x^3} \right) \right\}$$

$$\frac{\sqrt{\pi}}{2} \frac{1}{2} \frac{3 \cdot 5}{2 \cdot 2} - \frac{3\sqrt{\pi}}{4} \frac{1}{2}$$

~~.....~~ $\frac{-13}{16}$ $\frac{3}{8}$

$$= m_e n_e v_{the}^4 \left\{ \frac{v_{ei}}{\Omega_e^2} \frac{\nabla_{\perp} T_e}{T_e} \left(\frac{1}{2} - \frac{15}{16} \right) + \frac{2v_{ei}}{\Omega_e v_{the}^2 c n_e} \hat{b} \times \vec{j} \left(\frac{5}{8} - \frac{1}{4} \right) \right\}$$

So,

$$\vec{q}_\perp = - \underbrace{\frac{13}{4} \frac{n_e T_e}{m_e} \frac{v_{ei}}{\Omega_e^2} \nabla_\perp T_e}_{\perp \text{ heat conductivity} \equiv \kappa_\perp} + \underbrace{\frac{3}{2} T_e \frac{v_{ei}}{e \Omega_e} \hat{b} \times \vec{J}}_{\text{"Ettingshausen effect"}} \quad (301)$$

This is again diffusion but a different one than along the field.

$$\kappa_\perp \sim n_e v_{ei} \rho_e^2$$

So the step of the \perp random walk is ρ_e , not λ_{mp} — this is because electrons gyrate, so can't go very far across the field.

Key thing to carry from all this is that

$$\begin{aligned} \kappa_{||} &\sim n_e \frac{v_{the}^2}{v_{ei}} \\ \kappa_x &\sim \kappa_{||} \frac{v_{ei}}{\Omega_e} \\ \kappa_\perp &\sim \kappa_{||} \frac{v_{ei}^2}{\Omega_e^2} \end{aligned} \quad \left. \begin{array}{l} \text{progressively} \\ \text{smaller} \end{array} \right\} (302)$$

collisionless effect

basically because it is harder to move across \vec{B} than along it